

# ORIFICE METER

## BASIC SELECTION & DESIGN CONSIDERATIONS

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# METER SELECTION PHILOSOPHY

⌘ Reliability/ Repeatability

⌘ Rangeability

⌘ Versatility

⌘ Economics

⌘ Installation Cost

⌘ Maintenance cost

⌘ Easily Replaceable

⌘ Range modification

⌘ Space Occupation

# Why Orifice Meter

- Least Expensive.
- Easiest to Change.
- Locally Resizable.

# Why Orifice Meter (Continued)

METER	ERROR
•Single Orifice Meter	2%
•Dual Orifice Meter	0.75%
•Mag Flow meters	1%
•Positive displacement meter	0.25%

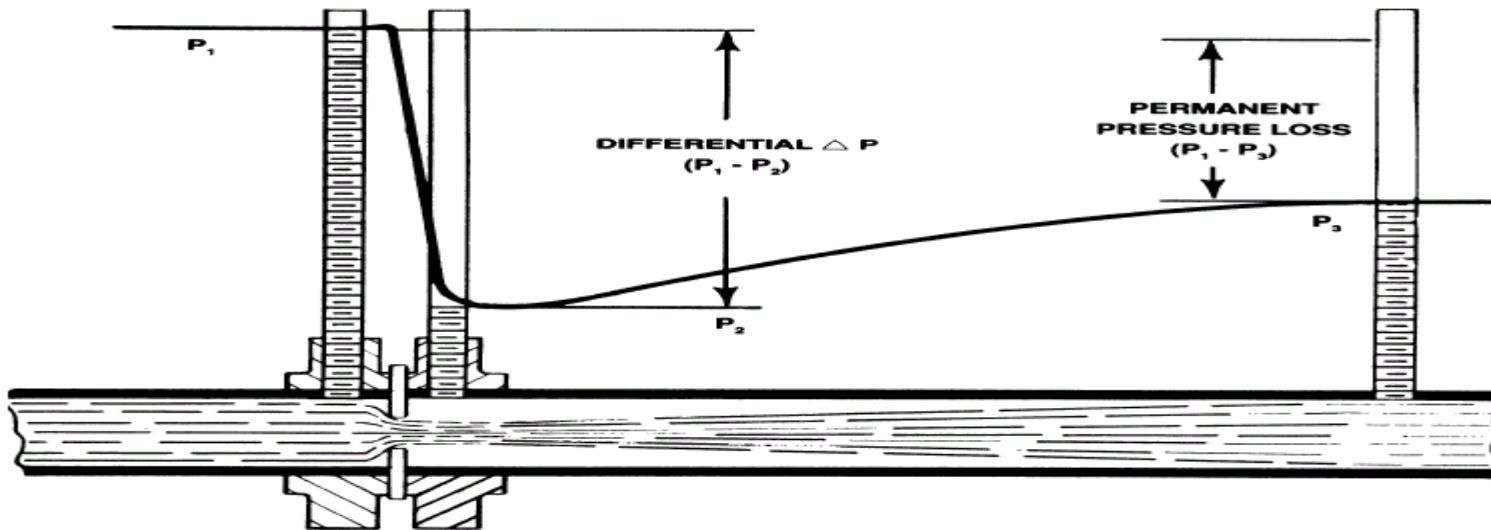
Therefore it is by far the most common sensing element used.

# What is an Orifice Meter?

An orifice Meter is a conduit and a restriction to create pressure drop.

# How does it work?

As the fluid approaches the orifice plate, the pressure increases slightly and then drops suddenly as the orifice plate is passed.



# CONCENTRIC ORIFICE PLATE SPECIFICATIONS

- Material of construction

SS-304, SS-316, or some special material

- Orifice plate Edge Thickness

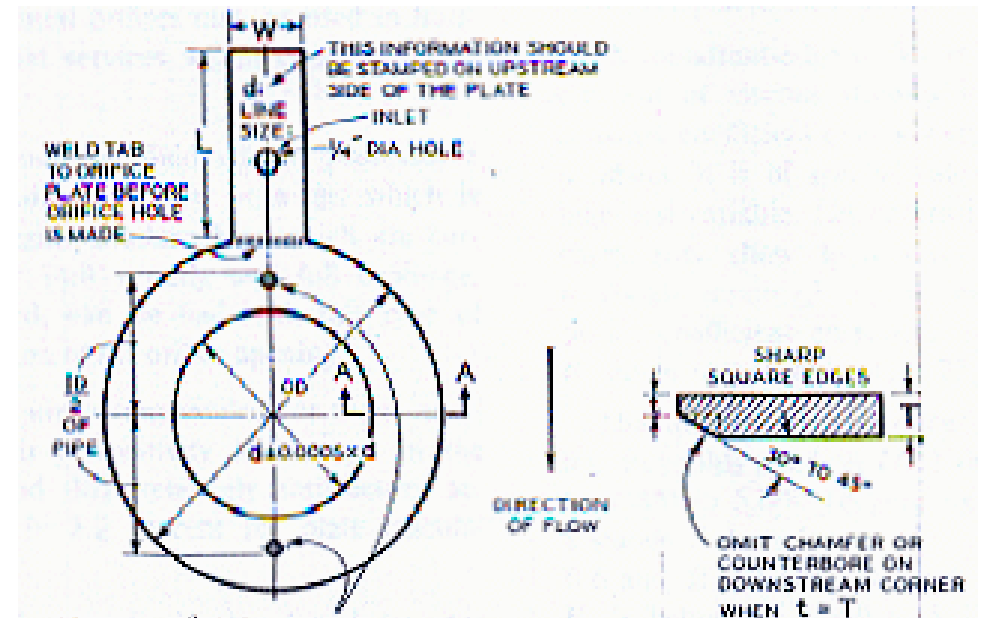
$D/50$ ,  $d/8$ ,  $(D-d)/8$

- The Upstream edge of Orifice

Square & Sharp

- Weep holes Provision

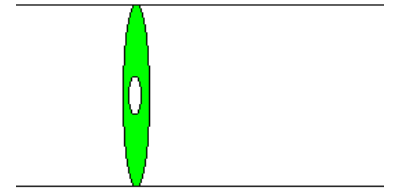
To remove moisture from wet steam, wet gas, or to remove non-condensables from liquid stream



# TYPES OF ORIFICE PLATE

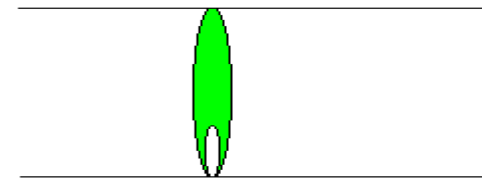
## A. The Thin Plate, Concentric Orifice

- Reliable measurement.
- The upstream edge of the orifice must be sharp and square.
- Minimum plate thickness based on pipe I.D., orifice bore, etc. is standardized.



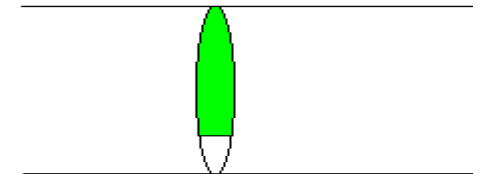
## B. Eccentric Orifice Plates

- ⌘ Round opening (bore) tangent to the inside wall of the pipe.
- ⌘ Used to measure fluids which carry a small amount of non-abrasive solids, or gases with small amounts of liquid.



## C. Segmental Orifice Plates

- ⌘ Used for measuring liquids or gases which carry non-abrasive impurities such as light slurries or exceptionally dirty gases.
- ⌘ Efficiency not as good as that of Concentric Plate.

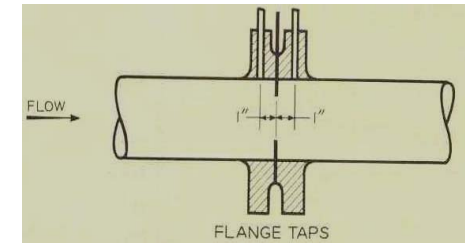




# METER TAP TYPE / LOCATION

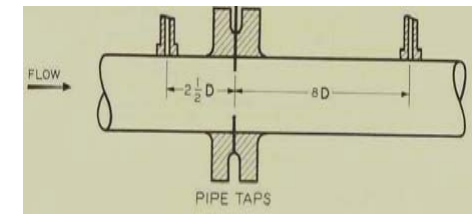
## a. Flange Taps

- 1" from the U/S face
- 1" from the D/S face with a + 1/64 to +1/32 tolerance.



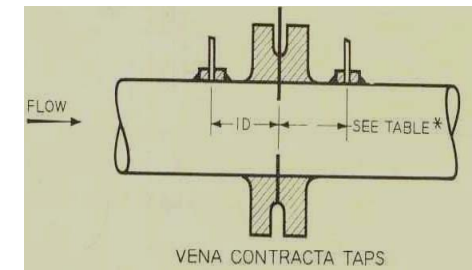
## b. Pipe Taps

- 2½ pipe diameters U/S
- 8 pipe diameters downstream  
(point of maximum pressure recovery).



## c. Vena-Contracta Taps

- One pipe diameter U/S
- The point of minimum pressure downstream  
(vena-contracta 0.3-0.8 PD).



## d. Corner Taps

- Immediately adjacent to the plate faces, U/S and D/S.
- Used in line sizes less than 2 inches

# TAP LOCATION / FLOW DIRECTION

- ⌘ Hold Impulse Leads to Min. Length
- ⌘ 1in/ ft positive slop to avoid possible pocketing & to provide venting / drainage.
- ⌘ In Vertical lines Up flow for liquids to avoid vap or Trash build up
- ⌘ Install meter Below the tap for liquids and condensable vapors
- ⌘ For gases install meter above the taps for avoiding the accumulation of condensable

# DESIGN CONSIDERATION OF ORIFICE METER

- Design Flow rate and Meter Capacity

Design flow should be above 30% and below 90% of maximum Flow.

- $\beta$  Ratio ( $d/D$ ) (Range varies between 0.7 to 0.25)
- Meter  $dP$  ( $<1/25$ th of the line pressure)
- Line Size (Minimum line size of 2" is standard because of pipe roughness considerations)

# Orifice Plate Coefficient of Discharge - Cd

The coefficient of discharge depends on

- ⌘ Reynolds number
  - ⌘ Sensing tap location
  - ⌘ Meter tube diameter
- &
- ⌘ Orifice diameter etc.

# SIZING ORIFICES

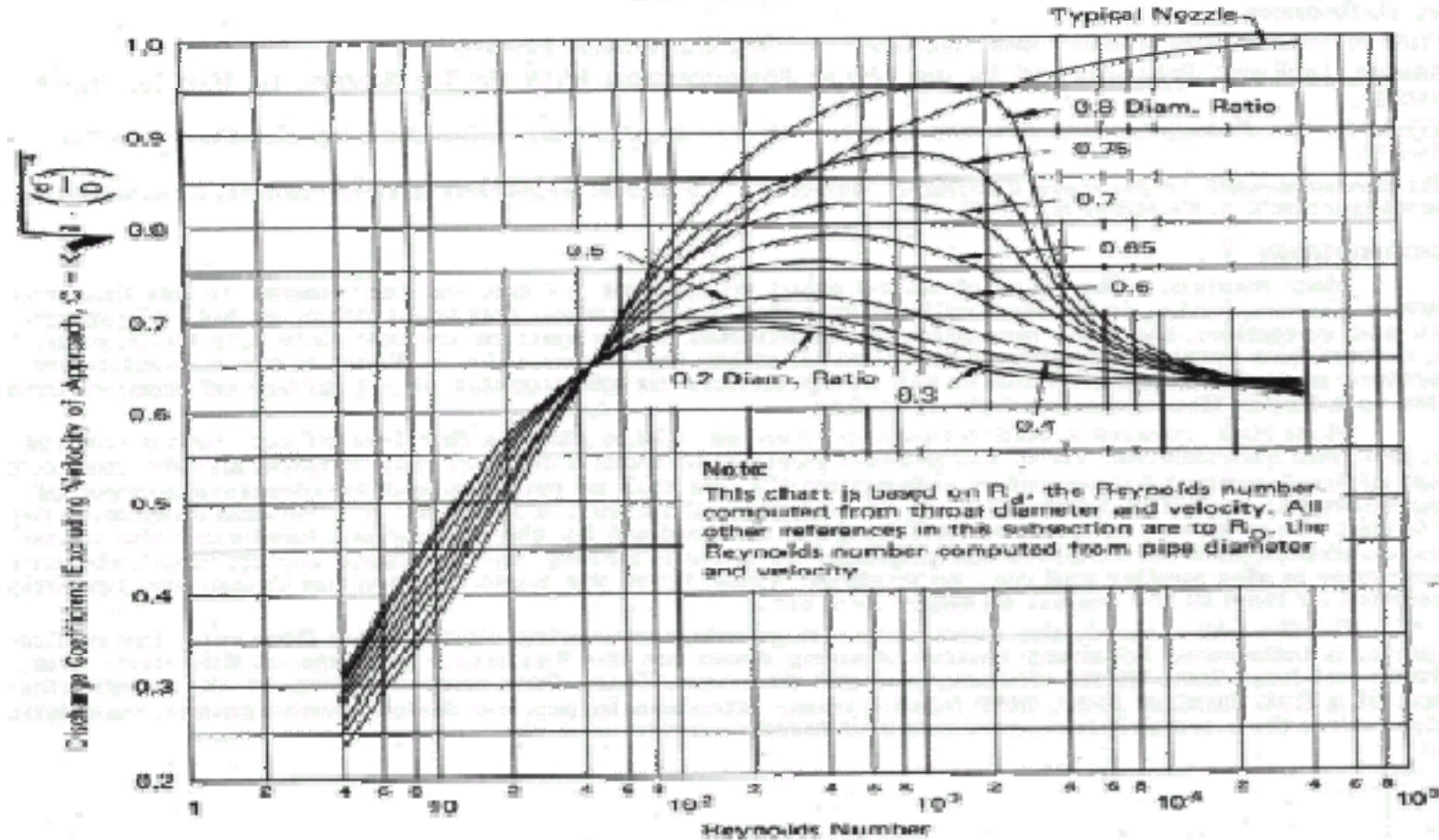
Orifice Plates are sized to provide the differential of 100~200 in H<sub>2</sub>O Column at maximum Flow Rate.

Advantage:

This sizing allows to change the meter range without changing the orifice plate.

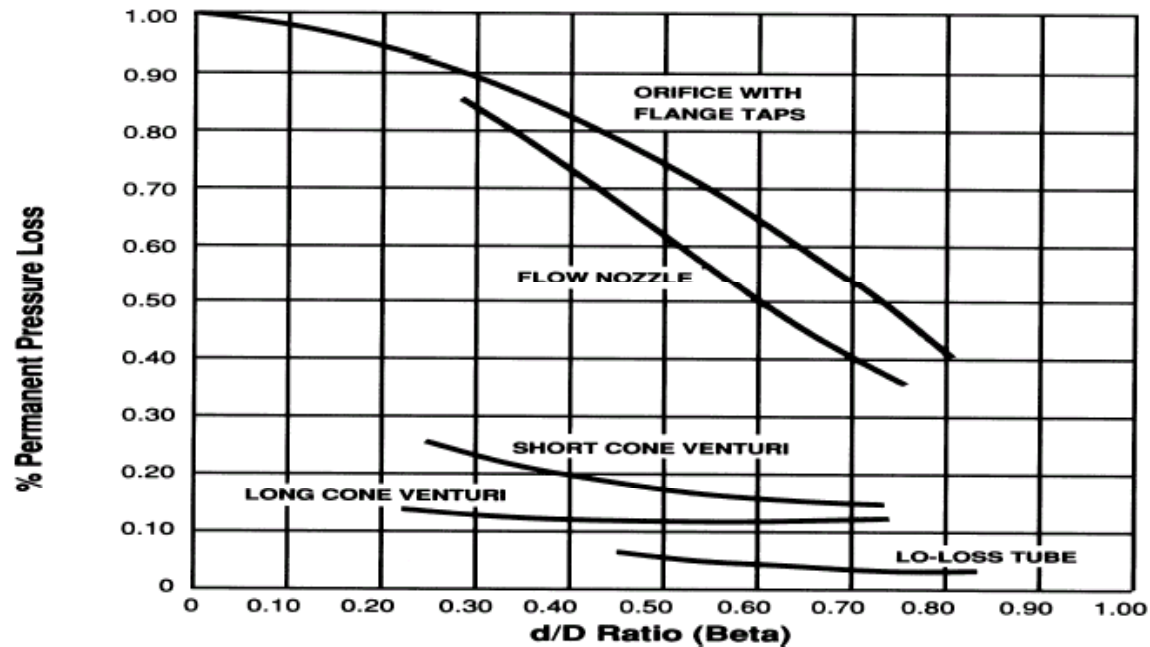
# Discharge Coefficient

DISCHARGE COEFFICIENTS FOR ORIFICES  
AND NOZZLES IN VISCOUS SERVICE  
WITH FLANGE TAPS



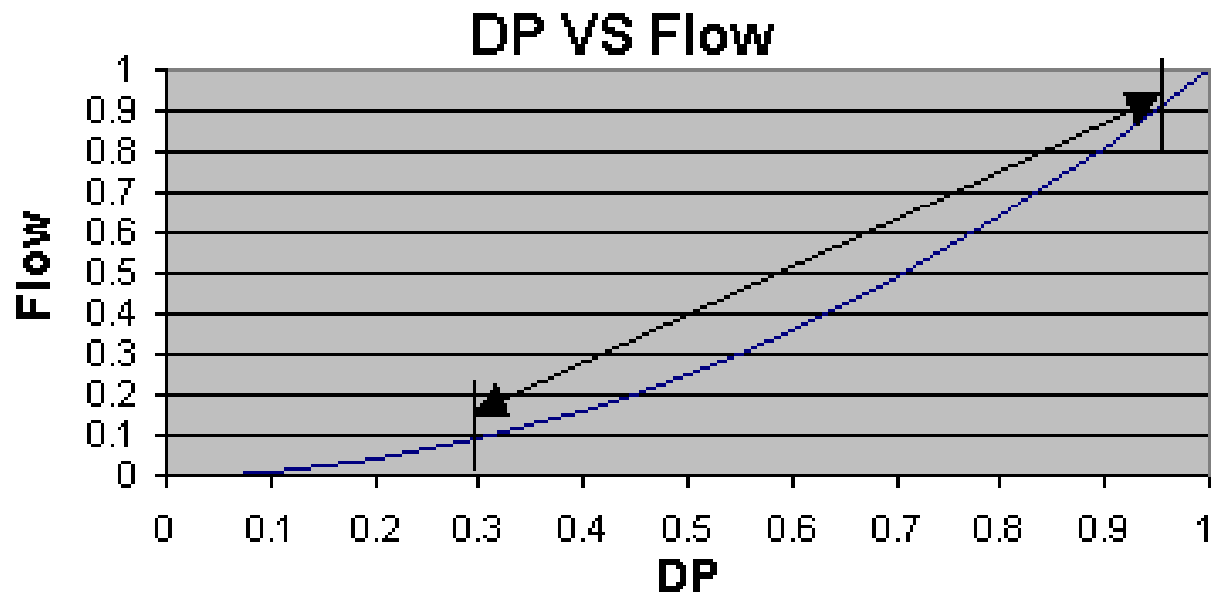
# Pressure Recovery

The fraction of the orifice differential that is lost permanently depends upon  $\beta$  ratio.



# Orifice Meter Limitations

RANGEABILITY:



Because of Sq. Root Relationship accuracy and readability become worse at decreased flow rates.



# Orifice Meter Limitations CONTINUED

RANGEABILITY :

Solution:

To decrease this rangeability without loss in accuracy, two differential pressure transmitters with different ranges can be connected across Orifice Plate.

# Orifice Meter Limitations CONTINUED

## VARYING DISCHARGE COEFFICIENT AT LOW $R_D$

Below a Pipe  $R_D$  of about 20,000, the basic discharge coefficient changes markedly with  $R_D$  and hence with flow rate.

Solution:

For this reason Either

- It is not used below  $R_D$  20,000. Or
- Specially designed to operate on flat portion of the curve ( $C_D$  VS  $R_D$ ) with the realization that accuracy would somewhat reduced.

# Orifice Meter Limitations CONTINUED

## VARYING PROCESS CONDITIONS

As the Process flow conditions deviate from the design conditions, flow indications become inaccurate.

### Solution:

To compensate this inaccuracy in the indication the correction factors are introduced into the flow measuring relation.

# Correction Factors for Compressible Fluids

Pressure correction

$$Q_2 = \sqrt{\frac{P_2}{P_1}} \times Q_1$$

Temperature correction

$$Q_2 = \sqrt{\frac{T_1}{T_2}} \times Q_1$$

Molecular weight Correction

$$Q_2 = \sqrt{\frac{M_2}{M_1}} \times Q_1$$

Overall Correction

$$Q_2 = \sqrt{\frac{P_2 M_2 T_1}{P_1 M_1 T_2}} \times Q_1$$

# Correction Factors for Compressible Fluids

## EXAMPLES

CO2 Flow to UR-1

Parameter

Design

Operating

Temp

95 F

95 F

Press

5 Psig

7 Psig

MW

44

43.65

Flow

510 KSCFH

533 KSCFH

# Correction Factors for Compressible Fluids

## EXAMPLES

CO2 Flow to UR-2

Parameter

Design

Operating

MW

44

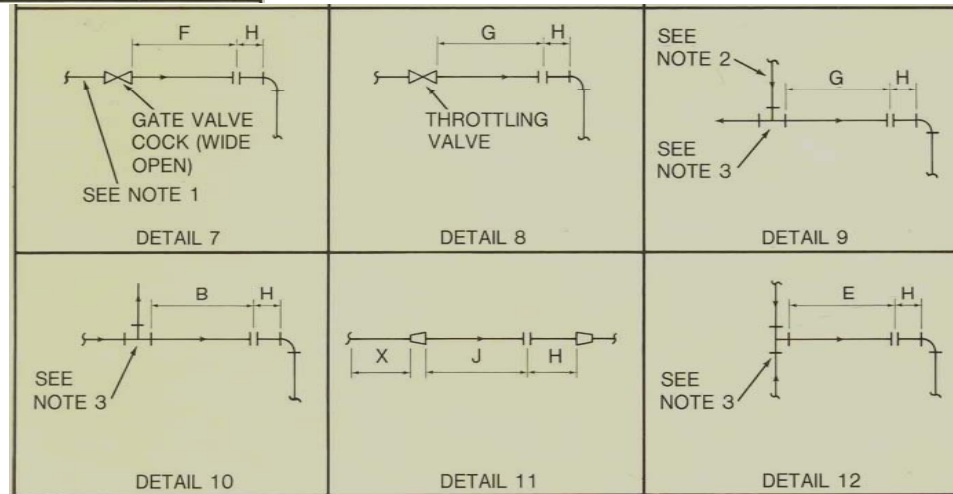
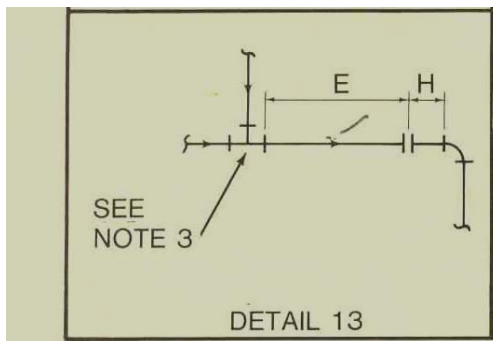
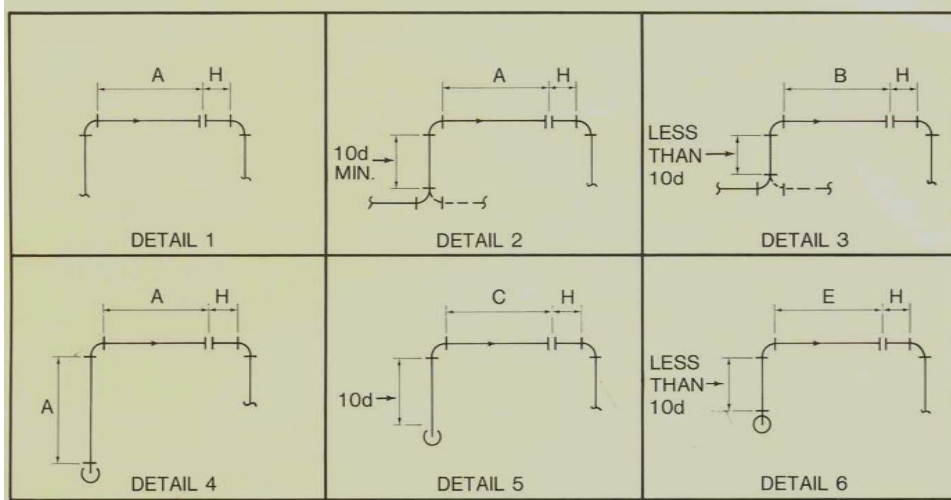
43.427

Flow

1280

1272

# Straight Run Vs Fittings



# Straight Run Vs Fittings

Table 1-2—d/D vs. Straight Run Required

Orifice ID d/D = Actual Pipe ID (See Note 4)	Straight Run Required (Nominal Pipe Diameters)							
	A	B	C	E	F	G	H	J
.8	20	25	33	40	14	50	5	15
.75 →	17	21	27	35	11	44	5 ✓	14
.7	14	19	23	31	9	39	5	13
.65	12	15	21	28	8	34	5	11
.6	10	14	19	25	8	31	5	10
.55	9	12	18	22	7	28	5	9
.5	8	10	17	21	7	25	5	8
.45	7	9	16	20	5	24	5	7
.4	7	9	15	18	5	22	5	7
.35	6	9	14	17	5	21	5	6
.3	6	9	14	16	5	20	5	6
.25	6	9	14	16	5	19	5	6

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# ORIFICE METER CALCULATIONS

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# BASIC EQUATIONS

$$\text{Liquid Flow} > M_L = 2834.53 * D^2 * \beta^2 * C_d * F_a * (Sp.g * H)^{1/2}$$

$$\text{Gas Flow} > M_G = 2834.53 * D^2 * \beta^2 * C_d * F_a * Y_1 * (\rho * H)^{1/2}$$

- ⌘  $C_d$  = Orifice plate coefficient of discharge
- ⌘  $D$  = Pipe ID calculated at Standard Conditions
- ⌘  $\rho$  = Density of Gas at reference conditions (Lb/Cu ft)
- ⌘  $H$  = Orifice differential pressure in inches of water at 60 degF
- ⌘  $Q_{L,G}$  = Mass flow rate - Lb/hr.
- ⌘  $Y_1$  = Expansion factor (upstream tap)
- ⌘  $F_a$  = Ratio of the Orifice bore area at operating conditions to those at 60 °F
- ⌘  $\beta$  = Ratio of Orifice Bore Dia to Pipe ID

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